

# A New Analytical Small-Signal Model of Dual-Gate GaAs MESFET

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**Abstract** — The development of an analytical small-signal model for the intrinsic elements of a dual gate GaAs MESFET (DGMESFET) is described. The model is based on splitting the Z-parameters of each FET part analytically without any simplifications or assumptions. The model is extracted directly from the measured three-port S-parameters. No extra measurements are required, thus reducing the lengthy procedures needed to characterize the DGMESFET. Experimental verification of the new model is presented.

## I. INTRODUCTION

THE dual-gate GaAs MESFET is involved in a wide range of applications. Several small-signal models of a DGMESFET have been reported [1]-[5]. The basic model of a DGMESFET is a cascode connection of two single-gate MESFET's, FET<sub>1</sub> and FET<sub>2</sub> [2]. To extract the intrinsic elements of DGMESFET, very lengthy procedures are required. Tsironis and Meirer [3] needed a dc bi-directional transfer characteristics [6], two-sets of two-port S-parameters measured at two different bias conditions, three-port S-parameters, and four levels of optimization, to extract the equivalent circuit elements of DGMESFET. The same procedures were carried out by Deng and Chu [7] but with only one level of optimization. Scott and Minasian [4] derived relationships between the three-port Z-parameters of the DGMESFET ( $Z$ ) and the individual two-port Z-parameters of the two single-gate FET's ( $Z^I$  and  $Z^{II}$ ). Except for  $Z_{22}^I$ , the two-port Z-parameters of FET<sub>1</sub> were given explicitly from the three-port Z-parameters of the DGMESFET. To separate  $Z_{22}^I$ , Scott and Minasian [4] assumed that up to moderate frequencies,  $Z_{22}^I \approx Z_{23}$ . Extracting the elements of FET<sub>1</sub> from its two-port Z-matrix, Scott and Minasian [4] found that the elements of FET<sub>2</sub> can be evaluated analytically

from the three-port Y-parameters of DGMESFET provided that the transconductance of FET<sub>2</sub> ( $g_{m2}$ ) is available. Measuring  $g_{m2}$  by using the model presented by Minasian [8], Scott and Minasian [4] derived expressions for extracting the elements of FET<sub>2</sub> under the assumptions that:

$$1 + j\omega C_{gs_1} R_{i_1} \approx 1; \text{ and } 1 + j\omega C_{gs_2} R_{i_2} \approx 1.$$

In this paper we derive an analytical expression of  $Z_{22}^I$  that can be evaluated from the measured three-port Z-parameters of the DGMESFET. Once  $Z_{22}^I$  is evaluated, the Z-matrix of each individual FET part is separated and the intrinsic elements of each FET can be evaluated analytically.

In the following, Section II describes the derivation of the  $Z_{22}^I$  analytical expression. In Section III, the experimental results using the analytical model are presented. Finally, the conclusion is presented in Section IV.

## II. DERIVATION OF $Z_{22}^I$ EXPRESSION

The typical intrinsic small-signal model of DGMESFET is shown in Fig. 1. For simplicity, Fig. 2. will be used, where the current sources and the admittances of each branch of the small-signal model are shown, and given by the following equations:

$$Y_1 = \frac{\omega^2 R_{i_1} C_{gs_1}^2}{E_1} + j \frac{\omega C_{gs_1}}{E_1} \quad (1)$$

$$Y_2 = j\omega C_{gd_1} \quad (2)$$

$$Y_3 = g_{d_1} + j\omega C_{ds_1} \quad (3)$$

$$Y_4 = \frac{1}{R_{12}} \quad (4)$$

$$Y_5 = g_{d_2} + j\omega C_{ds2} \quad (5)$$

$$Y_6 = j\omega C_{gd_2} \quad (6)$$

$$Y_7 = \frac{\omega^2 R_{i_2} C_{gs2}^2}{E_2} + j \frac{\omega C_{gs2}}{E_2} \quad (7)$$

$$G_1 = G_{1r} + jG_{1i} \quad (8)$$

$$G_2 = G_{2r} + jG_{2i} \quad (9)$$

where

$$E_1 = 1 + \omega^2 R_{i_1}^2 C_{gs1}^2$$

$$E_2 = 1 + \omega^2 R_{i_2}^2 C_{gs2}^2$$

$$G_{1r} = \frac{g_{m1}}{E_1} (\cos(\omega \tau_1) - \omega R_{i_1} C_{gs1} \sin(\omega \tau_1))$$

$$G_{1i} = \frac{-g_{m1}}{E_1} (\omega R_{i_1} C_{gs1} \cos(\omega \tau_1) + \sin(\omega \tau_1))$$

$$G_{2r} = \frac{g_{m2}}{E_2} (\cos(\omega \tau_2) - \omega R_{i_2} C_{gs2} \sin(\omega \tau_2))$$

$$G_{2i} = \frac{-g_{m2}}{E_2} (\omega R_{i_2} C_{gs2} \cos(\omega \tau_2) + \sin(\omega \tau_2))$$

When the inter-gate resistance  $R_{12}$  is taken into consideration, the three-port  $Z$ -parameters derived by Scott and Minasian [4] are modified as follows:

$$Z_{11} = Z_{11}^I$$

$$Z_{12} = Z_{12}^I$$

$$Z_{21} = Z_{21}^I$$

$$Z_{13} = Z_{13}^I$$

$$Z_{22} = Z_{22}^I + Z_{11}^{II} + R_{12}$$

$$Z_{23} = Z_{22}^I + Z_{12}^{II} + R_{12}$$

$$Z_{31} = Z_{21}^I$$

$$Z_{32} = Z_{22}^I + Z_{21}^{II} + R_{12}$$

$$Z_{33} = Z_{22}^I + Z_{22}^{II} + R_{12} \quad (10)$$

The two-port  $Y$  and  $Z$ -matrices of  $FET_1$  are given by:

$$Y^I = \begin{bmatrix} Y_1 + Y_2 & -Y_2 \\ G_1 - Y_2 & Y_2 + Y_3 \end{bmatrix} \quad (11)$$

$$Z^I = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22}^I \end{bmatrix} \quad (12)$$

Since  $Y = Z^{-1}$ , the following relationship results:

$$Y_2 = \frac{Z_{12}}{\det(Z^I)} \quad (13)$$

where

$$\det(Z^I) = Z_{11} Z_{22}^I - Z_{12} Z_{21}.$$

Similarly the two-port  $Y$  and  $Z$ -matrices of  $FET_2$  are:

$$Y^{II} = \begin{bmatrix} Y_6 + Y_7 & -Y_6 \\ G_2 - Y_6 & Y_5 + Y_6 \end{bmatrix} \quad (14)$$

$$Z^{II} = \begin{bmatrix} Z_{22} - R_{12} - Z_{22}^I & Z_{23} - R_{12} - Z_{22}^I \\ Z_{32} - R_{12} - Z_{22}^I & Z_{33} - R_{12} - Z_{22}^I \end{bmatrix} \quad (15)$$

It can be shown that:

$$Y_6 = \frac{Z_{23} - R_{12} - Z_{22}^I}{\det(Z^{II})} \quad (16)$$

where

$$\det(Z^{II}) = \alpha_1 - \alpha_2 Z_{22}^I$$

$$\alpha_1 = (Z_{22} - R_{12})(Z_{33} - R_{12}) - (Z_{23} - R_{12})(Z_{32} - R_{12})$$

$$\alpha_2 = Z_{22} + Z_{33} - Z_{23} - Z_{32}$$

It is clear from (2) and (6) that the real parts of both  $Y_2$  and  $Y_6$  are zeros. Solving  $\text{Re}(Y_2) = 0$  gives:

$$k_1 \text{Re}(Z_{22}^I) - k_2 \text{Im}(Z_{22}^I) = k_3 \quad (17)$$

where

$$\begin{aligned}
 k_1 &= \operatorname{Re}(Z_{11})\operatorname{Re}(Z_{12}) + \operatorname{Im}(Z_{11})\operatorname{Im}(Z_{12}) \\
 k_2 &= \operatorname{Im}(Z_{11})\operatorname{Re}(Z_{12}) - \operatorname{Re}(Z_{11})\operatorname{Im}(Z_{12}) \\
 k_3 &= \operatorname{Re}(Z_{12})\operatorname{Re}(Z_{12}Z_{21}) + \operatorname{Im}(Z_{12})\operatorname{Im}(Z_{12}Z_{21})
 \end{aligned}$$

Solving  $\operatorname{Re}(Y_6) = 0$  gives:

$$\begin{aligned}
 \beta_1(\operatorname{Re}^2(Z_{22}^1) + \operatorname{Im}^2(Z_{22}^1)) - \beta_2\operatorname{Re}(Z_{22}^1) + \beta_3\operatorname{Im}(Z_{22}^1) \\
 + \beta_4 = 0
 \end{aligned} \tag{18}$$

where

$$\begin{aligned}
 \beta_1 &= \operatorname{Re}(\alpha_2) \\
 \beta_2 &= \operatorname{Re}(\alpha_2)\operatorname{Re}(Z_{23} - R_{12}) + \operatorname{Re}(\alpha_1) \\
 &\quad + \operatorname{Im}(\alpha_2)\operatorname{Im}(Z_{23}) \\
 \beta_3 &= \operatorname{Im}(\alpha_2)\operatorname{Re}(Z_{23} - R_{12}) - \operatorname{Re}(\alpha_2)\operatorname{Im}(Z_{23}) \\
 &\quad - \operatorname{Im}(\alpha_1) \\
 \beta_4 &= \operatorname{Re}(\alpha_1)\operatorname{Re}(Z_{23} - R_{12}) + \operatorname{Im}(\alpha_1)\operatorname{Im}(Z_{23})
 \end{aligned}$$

Solving (17) and (18) results in:

$$\operatorname{Re}(Z_{22}^1) = \frac{-B - \sqrt{B^2 - 4AC}}{2A} \tag{19}$$

$$\operatorname{Im}(Z_{22}^1) = \frac{k_1\operatorname{Re}(Z_{22}^1) - k_3}{k_2} \tag{20}$$

where

$$\begin{aligned}
 A &= \beta_1 \left( 1 + \left( \frac{k_1}{k_2} \right)^2 \right) \\
 B &= \beta_3 \left( \frac{k_1}{k_2} \right) - \beta_2 - 2\beta_1 \frac{k_1 k_3}{k_2^2} \\
 C &= \beta_1 \left( \frac{k_3}{k_2} \right)^2 - \beta_3 \left( \frac{k_3}{k_2} \right) + \beta_4
 \end{aligned}$$

Once  $Z_{22}^1$  is evaluated from (19) and (20), the two-port Z-matrix of each individual single-gate FET is separated using (10). Converting the Z-matrix into a Y-matrix, the intrinsic elements of each FET part are evaluated using the well-established analytical model of single-gate FET [9].

### III. EXPERIMENTAL RESULTS

The model described in section II has been coded into a MATLAB program and is used to determine the intrinsic elements of the DGMESFET using the measurements published in [7]. Table I summarizes the extracted element values, with our model and compares these results with those obtained in [7]. It is clear that the extracted values are very close to those extracted by Deng and Chu [7], which verifies the validity of the new model.

TABLE I  
AVERAGE VALUES OF THE EXTRACTED INTRINSIC  
ELEMENTS OF DGMESFET

Elements	Average values using the new model		Average values using the model described in [7]	
	FET <sub>1</sub>	FET <sub>2</sub>	FET <sub>1</sub>	FET <sub>2</sub>
$C_{gs}$ (pF)	0.2194	0.2414	0.22	0.24
$R_i$ ( $\Omega$ )	6.431	8.96	6.44	9
$C_{gd}$ (fF)	64.583	59.78	64.3	60
$g_m$ (A/V)	0.0614	0.0251	0.0618	0.025
$\tau$ (ps)	7.21	7.71	7.2	7.7
$g_d$ (mS)	9.5	6.7	9.6	6.67
$C_{ds}$ (fF)	50.2	29.94	51	30

### IV. CONCLUSION

An analytical small-signal model of a dual-gate MESFET has been described. The two-port Z-matrix of each individual single-gate MESFET is separated analytically without any simplifications. The model is extracted entirely from the measured three-port S-parameters, with no need for extra measurements. The model gives unique solution to the intrinsic elements of the DGMESFET without lengthy procedures to extract those elements.

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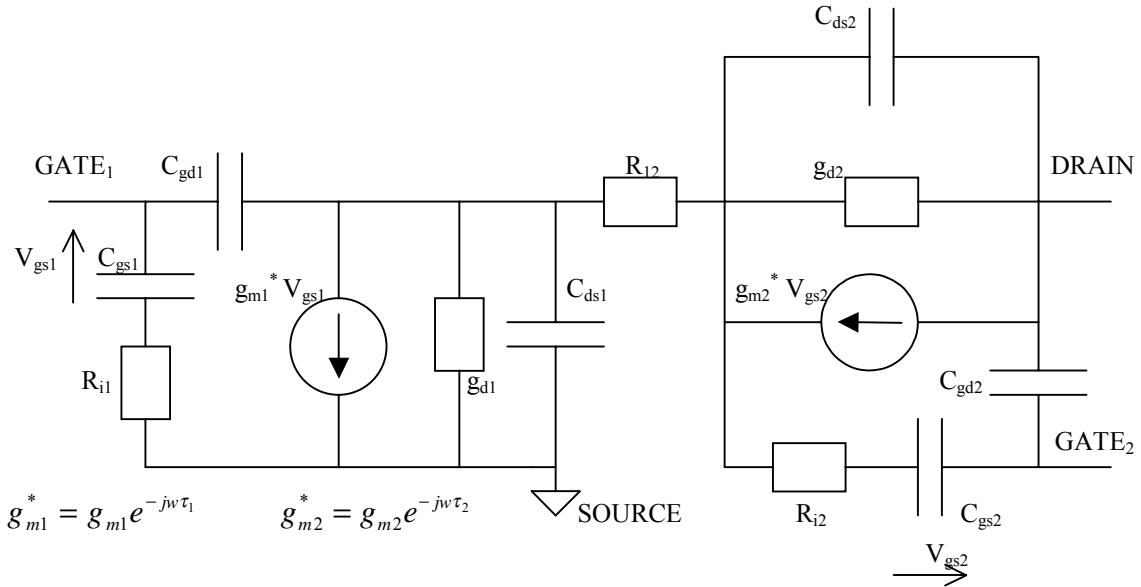


Fig. 1. The small-signal equivalent circuit of intrinsic DGMESFET.

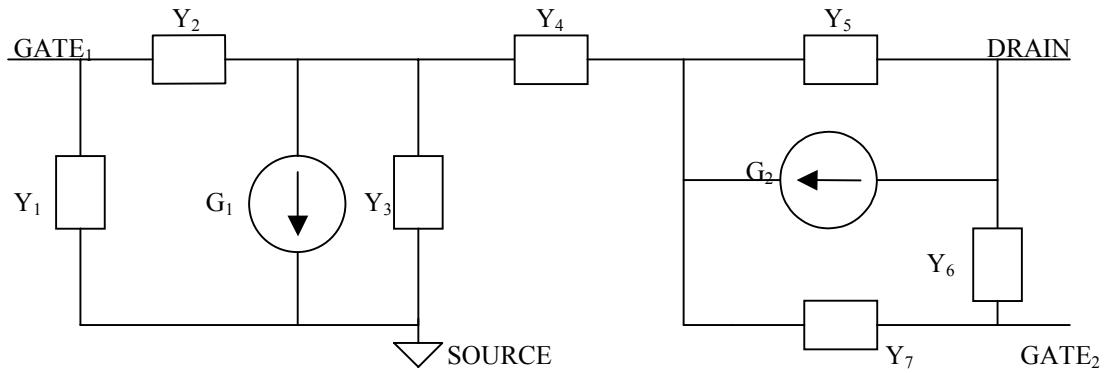


Fig. 2. The simplified equivalent circuit used for analysis.